Efficient Optimization Using Experimental Queries: A Peak-Search Algorithm for Efficient Load-Pull Measurements

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In the process of hardware optimization, physical queries requiring laboratory experiments are often necessary. This is similar to optimization using software where queries are made to a computer model. In both the laboratory optimization and optimization using computer models, queries come at a cost: laboratory time or computer time. Finding efficient searches using a small number of queries on average is therefore motivated. In this paper, techniques used in computer search are shown to be transparently applicable to certain instances of hardware optimization. The hardware example presented is a load-pull peaksearch algorithm for power amplifier load-impedance optimization. The successful search shown in this paper allows high-resolution measurement of the maximum power with a significant reduction in the number of measured reflection-coefficient states. The use of computationally intelligent procedures for reducing time costs in design optimization using hardware has significant potential applications in a number of iterative experimental procedures performed in the laboratory.

Keywords: load pull, steepest ascent, power, microwave, transistor

1. Introduction

In computer optimization using procedures such as genetic algorithms or hill climbing, the most computationally demanding operation is typically querying of a computer model. Thus, the query count is a metric for assessing the relative efficiency of one search algorithm over another. Search algorithms are also used in experimental optimization of hardware. Here, however, queries are made using physical laboratory measurements. The cost of a query here is laboratory time. For hardware requiring optimization of every unit, minimization of the number



o = Measured Reflection Coefficient State

Fig. 1. Measured 3.5 GHz load-pull results for $P_{in} = 14.5$ dBm at $V_{GS} = -0.7$ V, $V_{DS} = 10$ V.

of queries per optimization has a multiplicative effect on the unit cost. An example is optimization of impedance loading conditions for maximum output power in amplifier design. Load-pull measurements are often used to find optimal impedance loading conditions for power amplifier design. In traditional microwave load-pull measurements, a number of reflection-coefficient states are pre-selected and measured. Contours of equal power are then fitted to the results, as shown in Fig. 1. In the measurement displayed, 43 different reflection-coefficient states are chosen. Approximately 4 sec are required for each measurement, requiring a total of nearly 3 min to complete the measurement. This often is not fast enough for cases in which devices must be load-pulled multiple times in order to find the maximum Power-Added Efficiency (PAE) and gain at optimum loading conditions over variations in bias, process, and often input power. This creates a demand for a better search. The purpose of this paper is to demonstrate the application of steepest ascent to a loadpull search designed to minimize the number of queries required for reflection-coefficient optimization.

Using software emulation of device physics of a GaAs *Pseudomorphic High Electron Mobility Transistor* (PHEMT) [1, 2], the authors have previously shown that a steepest ascent procedure significantly reduces the number of queries required for optimization. In addition to reducing characterization time in the laboratory, these methods can be used in on-chip load-pull to determine the optimum loading condition for a new frequency range [3].

In searching for the best search to use in this problem, several methods have been presented in the literature. Perlow has described an algorithm that uses multiple measurements to determine the location of a contour and then, from this, ascend [4]. De Hek et al. have described a method that begins with measured points at a significant radius on the Smith Chart and calculates the location and value of the maximum power from a function fit to the data points. The search is repeatedly reiterated at smaller radii until the solution converges with respect to power and Smith Chart location for decreasing radius of the measurements [5]. A genetic algorithm was employed by Qiao et al. for on-chip optimization of a reconfigurable power amplifier [3], but such algorithms are prone to require a significantly larger number of queries than the steepest ascent method, consistent with the conclusions of Copalu [6] that the steepest ascent method is often advantageous because it can work under arbitrary criterion functions.

2. The Steepest-Ascent Algorithm for Load-Pull

The problem at hand is the optimization of the change in output power (relative to the starting point) over changes in the real and imaginary parts of the load reflection-coefficient: $\Delta P(\Delta \Gamma_r, \Delta \Gamma_i)$. The desire is to choose, with as few queries as possible, the combination of real and imaginary part of the load reflectioncoefficient $(\Delta\Gamma_r, \Delta\Gamma_i)$ that maximizes the output power delivered from the transistor to the load. For this optimization, the criterion is output power, and the parameters to be adjusted to optimize the criterion are the real and imaginary parts of the load reflection-coefficient $\Delta\Gamma_r$ and $\Delta\Gamma_i$, respectively. The variables $\Delta\Gamma_r$ and $\Delta\Gamma_i$ can thus be plotted on a *Smith Chart* as used, for example, in Fig. 1. Varying the complex load reflection-coefficient throughout the Smith Chart and measuring at different reflectioncoefficients in order to optimize output power is known as "load-pull." The search described in this section is designed to minimize the number of queries necessary to find the optimum-power combination of $\Delta\Gamma_r$ and $\Delta\Gamma_i$.

The search is divided into initial and final stages [7]. Two neighboring points are measured in each direction about the starting point at a distance D_n , changing only one of the coordinates for each point, as shown in **Fig. 2**. From these three measurements, an equation for a plane



Fig. 2. Measurements to extract tangent plane equation and direction of steepest ascent.



Fig. 3. Measurement of power at a new candidate point.

tangent to the response at the starting point can be constructed:

$$\Delta P(\Delta \Gamma_r, \Delta \Gamma_i) = m_1 \Delta \Gamma_r + m_2 \Delta \Gamma_i. \quad . \quad . \quad . \quad (1)$$

From measurements of power at the candidate and the two nearest neighbors (as shown in **Fig. 2**), two values of ΔP are obtained by subtracting the power at the candidate point from the power at both of the nearest neighbors. Substituting these values of ΔP and the associated values of $\Delta \Gamma_r$ and $\Delta \Gamma_i$ in Eq. (1) can be used to solve for m_1 and m_2 . By setting $\Delta P = 0$, the equation for the line tangent to a contour of equal power is found to be

The equation for the line in the direction of the maximum rate of increase is perpendicular to the line of Eq. (2a) and is thus

$$\Delta\Gamma_i = \frac{m_2}{m_1} \Delta\Gamma_r. \qquad \dots \qquad \dots \qquad \dots \qquad \dots \qquad (2)$$

 D_s , the search distance, is the predetermined distance from the present candidate point to the subsequent candidate point. The next candidate point is found by proceeding a distance D_s to the next candidate point along the line of steepest ascent. It lies on the intersection of the circle

with the steepest-ascent line in Eq. (2). There are be two solutions for the intersection point, as the line of steepest ascent also serves as the line of steepest descent if followed in the opposite direction. The intersection point solution having a value of $\Delta P > 0$ from Eq. (1) is selected the second candidate point, as shown in **Fig. 3**. This point is then measured, and if a power increase is obtained, then the process is repeated for Candidate 2. If not, the search distance D_s is decreased to one-third of its initial value and another candidate is measured. The search proceeds to its conclusion when D_s falls below a predefined threshold.

At the end of the search (when $D_s < D_n$), five points are chosen around the final candidate point to extract



Fig. 4. Implementation of the final search stage.

a second-order polynomial approximation in the two reflection-coefficient variables:

$$\Delta P = m_1 \Delta \Gamma_r + m_2 \Delta \Gamma_i + \frac{1}{2} [m_{11} (\Delta \Gamma_r)^2 + 2m_{12} (\Delta \Gamma_r) (\Delta \Gamma_i) + m_{22} (\Delta \Gamma_i)^2] \quad . \quad . \quad . \quad (4)$$

Eq. (4) is a traditional second-order polynomial approximation in the two variables $\Delta \Gamma_r$ and $\Delta \Gamma_i$. A second-order equation is necessary to allow a maximum of the function to exist. This is important because the equation will be used to calculate both the power that can be delivered by the device and the combination of $\Delta\Gamma_r$ and $\Delta\Gamma_i$ that provide this maximum power. The candidate points used here are the points taken four directions from the center point (the points to the right and left of the center point will have already been measured at this point in the search), along with a fifth point that can be selected by the algorithm. The maximum of this function can be calculated by setting the gradient of Eq. (4) equal to zero and solving for $\Delta \Gamma_r$ and $\Delta \Gamma_i$, and then finding the associated value of ΔP from Eq. (4). Fig. 4 shows an intuitive description of the final search stage.

Because Perlow's algorithm [4], while being a steepestascent type, spends many measurements finding the equipower contour rather than searching for the steepest ascent direction, the method presently proposed based on [7] generally uses fewer measurements than the Perlow method. Because the method of de Hek [5] utilizes a "zoom-in" approach from the edge of the Smith Chart toward the center, it allows many measurements during its initial stages in regions of the Smith Chart far away from the optimum point, some of which could provide damage to the device due to the large power mismatch. Berghoff et al. [8] have proposed a method in which the phase and attenuation of the load tuner are iteratively optimized one at a time; however, optimizing one variable at a time may not result in finding the maximum¹ [7].

3. Algorithm Simulation Results

The initial testing of the accuracy and efficiency of this algorithm were performed by using MATLAB to control load-pull simulations in Agilent Technologies' Advanced Design System (ADS) software [9]. Simulation results are briefly reviewed here [1]. **Fig. 5(a)** shows traditional load-pull simulation contours of equal output power for a GaAs Pseudomorphic High Electron Mobility Transistor



Fig. 5. (a) Load-pull search path from MATLAB/ADS algorithmic implementation with output power contours generated from traditional ADS load-pull simulation, and (b) search algorithm progress for five different starting points.

 Table 1.
 MATLAB/ADS simulation results for different searches.

Starting Γ_L	Maximum Output Power Γ_L	Maximum Output Power	Number of Sim. Points
		(dBm)	
0 + j0	$0.689 < 90.05^{\circ}$	22.7184	17
0.5 + j0.5	$0.690 < 90.14^{\circ}$	22.7178	17
0.5 - j0.5	$0.690 < 90.05^{\circ}$	22.7154	19
$-0.5 - j \ 0.5$	$0.690 < 90.05^{\circ}$	22.7154	17
-0.4 + j0.4	$0.694 < 89.98^{\circ}$	22.7143	14

(PHEMT) model. Fig. 5(b) shows a plot of the candidate points and the search algorithm paths traversed from five different starting points. It can be seen that, for each of these starting points, the algorithm converges to essentially the same reflection-coefficient value for the maximum power; in addition, this point is identical to the maximum-power reflection-coefficient seen in Fig. 5(a). The MATLAB/ADS co-simulation found the maximum power for the HEMT model to be 22.72 dBm with simulation of only 17 reflection-coefficient states, while a simulation using a traditional ADS load-pull simulation with 400 different values of Γ_L found the maximum power to be 22.76 dBm. Table 1 shows the starting reflectioncoefficient, the final reflection-coefficient, the maximumpower reflection-coefficient, the maximum power, and the number of simulated states for each starting point in the peak searches performed.

Each search results in a maximum-power value and reflection-coefficient that should ideally be identical to the results from the other searches. The maximum reflection coefficient of each search corresponds to an impedance that can, in general, be represented by a series resistance R_{max} and capacitance C_{max} :

$$Z_{\max} = Z_0 \frac{1 + \Gamma_{\max}}{1 - \Gamma_{\max}} = R_{\max} - j \frac{1}{\omega C_{\max}} \quad . \quad . \quad (5)$$

The standard deviation in both the equivalent optimum

^{1.} The authors are presently developing methods to protect potentially unstable devices from going into oscillation during the load-pull search.

resistance R_{max} and the equivalent optimum capacitance C_{max} are useful measures of the variation of optimum end-point locations across the different searches. These can thus be used to assess the repeatability of the optimum endpoint. The standard deviation of the power value allows a measure of the repeatability of the optimum criterion value over the different searches. For the results shown, the optimum load resistance and capacitance mean and standard deviation have been found. The mean load resistance is 17.705 Ω with a standard deviation of 0.101 Ω , while the equivalent load capacitance is -3.407 pF with a standard deviation of 0.5738 fF. Excellent agreement has been achieved for the optimal load impedance despite different starting points for the search iterations.

4. Algorithm Measurement Results

Measurement testing involved the development and use of a MATLAB graphical user interface to control the Maury Microwave ATS Version 400 load-pull system and software [10]. The measurement system includes a loadpull tuner that is adjusted to desired values of Γ_L to the device output, and a power meter to measure the output power for each value of Γ_L . Fig. 6(a) shows the traditional load-pull results, with contours of equal output power and the maximum-power reflection-coefficient identified. Fig. 6(b) shows the maximum point identified by the peak-search algorithm, along with four different starting points used in the testing and the number of measurement queries necessary to obtain the optimum when starting from these points. It can be seen that, even from significant distances from the optimum, the search converges with a small number of queries.

As in the simulation case, the robustness of the measurement search results for different starting points on the Smith Chart was tested. **Table 2** shows the $P_{in} =$ 14.5 dBm (1-dB compression) search results for the use of the four different starting impedances shown in **Fig. 6(b**). The mean value of resistance (R_{max}) was found to be 44.283 Ω , with a standard deviation of 1.443 Ω . The capacitance (C_{max}) was found to have a mean value of -679.8 femto Farads (fF), with a standard deviation of 17 fF. The mean power value was found to be 28.311 dBm, with a standard deviation of 0.011 dBm. All four maximum power values are within 0.03 dBm of each other. These metrics all demonstrate excellent correspondence between results in the microwave measurement field.

5. Power-Swept Load-Pull

The value of Γ_L providing maximum output power migrates as the device moves from small-signal to largesignal operation. As the input power is increased, the values of maximum-power Γ_L at different power levels can be recorded and plotted on a Smith Chart. This provides



Fig. 6. (a) Traditionally measured load-pull results and (b) algorithm-measured load-pull results and different starting points used.

Table 2. Measurement results for different starting reflection-coefficients at $P_{in} = 14.5$ dBm.

Starting	Maximum	Maximum	Number
Γ_L	Output Power	Output	of
	Γ_L	Power (dBm)	Queries
0 + j0	0.233<86.1°	28.2962	18
0.5+j0.5	0.246<89.9°	28.3132	14
0.5-j0.5	0.261<92.0°	28.3220	23
-0.6-j0.5	0.256<90.7°	28.3134	23

measured data that can be used as another means of verifying the behavior of a nonlinear transistor model.

Based on the demonstrated correspondence obtained between algorithm-driven measurements and the traditional load-pull measurements, a series of maximum power searches was performed with the algorithm at different input power values. **Table 3** shows the search algorithm results for the different input power values. All searches were performed with a starting reflectioncoefficient of 0 + j0.

Table 3. Search algorithm measurement results for different input power values with a starting reflection coefficient of 0 + j0.

Pin	Maximum	Maximum	#
(dBm)	Output Power Γ_L	Output	Queries
		Power (dBm)	
-7	$0.488 {<} 53.0^{\circ}$	9.9242	24
0	$0.517 {<} 49.2^{\circ}$	15.6327	18
5	$0.534 < 54.5^{\circ}$	20.3879	21
10	0.436<64.4°	25.8117	27
12	$0.300 < 75.4^{\circ}$	27.4354	18
13	$0.283 < 85.4^{\circ}$	27.8654	18
14	0.197<101°	28.1543	21
14.5	$0.194 {<} 88.4^{\circ}$	28.3264	24
15.5	0.233<83.9°	28.8281	21
16.7	0.200<84.0°	28.8479	15



Fig. 7. Measured (upper curve) and simulated (lower curve) maximum-power reflection-coefficient for varying input power levels: -7, 0, 5, 10, 12, 13, 14, 14.5, 15.5, and 16.7 dBm.

To compare with the measured data shown in **Table 3**, simulations were performed for these input power values using an Angelov/Chalmers model [11], extracted by the authors for the PHEMT using pulsed IV, S-parameter, power sweep, and load-pull data. **Fig. 7** shows the measured and simulated migration of the maximum-power load reflection-coefficient with increasing input power. The model predicts the migration of the maximum-power reflection-coefficient with notable accuracy. This type of comparison is insightful because it shows the performance of the model at low power, high power, and medium power conditions.

To decrease the time of the power-swept load-pull measurement, a MATLAB script has been developed to run the sequence of searches more efficiently. A starting Γ_L value is specified for the first search (this would be the -7 dBm case in the above example). The maximum-

Table 4. Starting point, ending point, and number of queriesfor each search in the maximum-power impedance migrationsimulation.

Pin	Starting Γ	Ending Γ	Max	# Overies
			(dBm)	Queries
-7	$0{<}0^{\circ}$	$0.48{<}44.8^{\circ}$	8.40	12
0	$0.48 {<} 44.8^{\circ}$	$0.51 < 44.0^{\circ}$	15.28	6
5	$0.51 < 44.0^{\circ}$	$0.50 {<} 45.8^{\circ}$	20.18	6
10	$0.50 {<} 45.8^{\circ}$	$0.37 < 56.6^{\circ}$	25.17	15
12	$0.37 < 56.6^{\circ}$	$0.28 {<} 68.4^{\circ}$	26.78	12
13	$0.28 < 68.4^{\circ}$	$0.25 < 76.2^{\circ}$	27.46	12
14	$0.25 < 76.2^{\circ}$	0.23<84.5°	28.05	9
14.5	$0.23 < 84.5^{\circ}$	$0.22 < 88.7^{\circ}$	28.31	6
15.5	$0.22 < 88.7^{\circ}$	0.20<96.1°	28.76	9
16.7	0.20<96.1°	$0.17 < 102^{\circ}$	29.15	9

power Γ_L value from the first search is used as the starting point for the second search, and this trend is followed for all input power values to reduce the number of experimental queries. **Table 4** shows results for this "superalgorithm," and it can be seen that the maximum number of experiments performed occurs in the first search. Only a small number of points is required for most of the subsequent searches. The number of Γ_L points ("# Queries") evaluated for each input power is decreased from **Table 3**, where a separate search was performed for each Γ_L .

6. Conclusions

Search algorithms are designed to produce better and better values of fitness through repeated queries to an oracle. Since queries come at a cost, search procedures are needed that require a small number of queries to achieve success. Although most searches are performed using a computer software oracle, the same search paradigms can be applied to the cases of experimental optimization.

This work demonstrates that search algorithms used in computer search can be applied to find efficient methods that allow a reduced number of experimental calibration queries. The search chosen provided a significant improvement over a traditional load-pull measurement.

Steepest ascent has a significant history in optimization [12]. This paper has demonstrated measurement results of an application of this work that will significantly save microwave engineers time and money by decreasing measurement queries in bench-top testing of devices.

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