

# Holographic representation of space-variant systems: system theory

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System theory for holographic representation of linear space-variant systems is derived. The utility of the resulting piecewise isoplanatic approximation (PIA) is illustrated by example application to the invariant system, ideal magnifier, and Fourier transformer. A method previously employed to holographically represent a space-variant system, the discrete approximation, is shown to be a special case of the PIA.

## I. Introduction

By holographically recording an arbitrarily complex linear space-invariant system's transfer function, one may duplicate input-output relationships of the system with access solely to the hologram. An arbitrary input is Fourier transformed by a thin lens, multiplied by the holographically recorded transfer function placed in the lens's back focal plane, and reimaged. The output is equivalent to that of the recorded system with the same input. This type of system representation may be used to condense a multielement space-invariant linear system into a single hologram.

Unfortunately, there are many common optical systems of interest that are space variant to which this scheme cannot be directly applied. Recent efforts to holographically record space-variant systems employing a variation of the transfer function method, however, have proven successful. Either by input isoplanatic patch division or sampling, successful volume hologram' representations of the space-variant nonunity magnification imaging system have been obtained.<sup>1-5</sup>

It is thus of practical importance to investigate that system theory necessary for holographically representing space-variant systems. The approach employed herein divides the space-variant system input plane into isoplanatic patches to which corresponding transfer functions are assigned. The resulting piecewise isoplanatic approximation (PIA) output is

representative of the true system output. Although the isoplanatic patch concept is not new,<sup>6</sup> its use has been primarily confined to system analysis within a single patch.

The PIA is herein derived, and examples of its application to various systems are offered. Equivalence of true and PIA outputs of space-invariant systems is established. The discrete approximation (DA) previously employed for space-variant system representation<sup>1</sup> is shown to be a special case of the PIA.

## II. Foundations

For notational and continuity purposes, a brief review of classical linear system theory is now offered after Goodman.<sup>7</sup> Analysis is restricted to one dimension with no loss of generality.

A general system consisting of an input, a black box, and an output may be modeled by the mathematical operator  $\mathbf{S}[\ ]$  such that

$$g_0(x) = \mathbf{S}[g_i(x)], \quad (1)$$

where  $g_0(x)$  is an output corresponding to an input  $g_i(x)$ . A system is said to be linear if and only if

$$\mathbf{S}[ag_i(x) + bf_i(x)] = a\mathbf{S}[g_i(x)] + b\mathbf{S}[f_i(x)], \quad (2)$$

where  $a$  and  $b$  are constant. Such systems may be described by the superposition integral

$$g_0(x) = \int_{-\infty}^{\infty} g_i(\xi)h(x - \xi; \xi)d\xi, \quad (3)$$

where, after the notation of Lohmann and Paris,<sup>8</sup>

$$h(x - \xi; \xi) = \mathbf{S}[\delta(x - \xi)] \quad (4)$$

is the system's line spread function, and  $\delta(x)$  is the Dirac delta.

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Substituting into Eq. (17) and employing the shorthand notation of Eq. (7) give

$$g_0(x) = \sum_n g_n(x - x_n) * h_n(x) \quad (19a)$$

or equivalently

$$g_0(x) = \sum_n g_n(x) * h_n(x - x_n). \quad (19b)$$

The input-output relationship of a piecewise isoplanatic system can thus be expressed as a superposition of convolutions.

Equations (19a) and (19b) may also be expressed in the frequency domain as

$$G_0(f_x) = \sum_n G_n(f_x) H_n(f_x) \exp(-j2\pi f_x x_n), \quad (20)$$

where  $G_n(f_x)$  and  $H_n(f_x)$  are the respective Fourier transforms of  $g_n(x)$  and  $h_n(x)$ .

The power of the input-output relationship of a piecewise isoplanatic system lies in its use for synthesizing outputs of variant systems modeled as piecewise isoplanatic. Such a system model output will be called the Piecewise Isoplanatic Approximation (PIA). Note that the superposition integral [Eq. (3)] can be written

$$g_0(x) = \sum_n \int_{l_n}^{u_n} g_i(\xi) h(x - \xi; \xi) d\xi. \quad (21)$$

The PIA of the same system,  $\tilde{g}_0(x)$ , can be written

$$\tilde{g}_0(x) = \sum_n \int_{l_n}^{u_n} g_i(\xi) h(x - \xi; x_n) d\xi. \quad (22)$$

One sees that as each isoplanatic patch width narrows around  $x_n$  (matched by an increase in the number of patches), the PIA [Eq. (22)] approaches the true output  $g_0(x)$ .

## B. Examples

### 1. Invariant Systems

Application of the PIA to invariant systems gives the true output since invariant systems are indeed piecewise isoplanatic. For such systems, the invariance criterion of Eq. (5) is true. Substituting into the PIA [Eq. (19a)] and recognizing the distributive property of the convolution operator give

$$\begin{aligned} \tilde{g}_0 &= h(x) * \left[ \sum_n g_n(x - x_n) \right] \\ &= h(x) * g_i(x) \\ &= g_0(x). \end{aligned} \quad (23)$$

The true and approximated outputs are thus equivalent.

Consider as a specific example the differentiator with an input-output relationship of

$$g_0(x) = (d/dx)g_i(x). \quad (24)$$

The corresponding line-spread function is

$$h(x - \xi) = \delta'(x - \xi), \quad (25)$$

where  $\delta'(x)$  is the unit doublet, the first derivative of the Dirac delta. By the criterion of Eq. (5), the differentiator is invariant.

Substitution of Eq. (25) into the PIA [Eq. (19b)] yields

$$\begin{aligned} \tilde{g}_0 &= \sum_n g_i(x) \mu(x - l_n) \mu(u_n - x) * \delta'(x) \\ &= \sum_n \frac{d}{dx} g_i(x) [\mu(x - l_n) - \mu(x - u_n)] \\ &= \sum_n \mu(x - l_n) \mu(u_n - x) \frac{d}{dx} g_i(x) \\ &\quad + g_i(l_n) \delta(x - l_n) - g_i(u_n) \delta(x - u_n). \end{aligned} \quad (26)$$

In the above summation, the unwanted delta terms are canceled by corresponding delta terms in adjacent patches as specified in Eq. (12). This reduces Eq. (26) to

$$\begin{aligned} g_0(x) &= \sum_n \mu(x - l_n) \mu(u_n - x) \frac{d}{dx} g_i(x) \\ &= \frac{d}{dx} g_i(x), \end{aligned} \quad (27)$$

which is the desired result.

### 2. Ideal Magnifier

The ideal magnifier (imaging system) has an input-output relationship of

$$g_0(x) = (1/M)g_i(x/M). \quad (28)$$

The corresponding line-spread function is then

$$h(x - \xi; \xi) = \delta(x - M\xi). \quad (29)$$

Note that no mathematical manipulation may be performed on Eq. (29) to meet the invariance criterion of Eq. (5) except for the trivial case of unity magnification. Thus, in the classical sense, the magnifier is space variant.<sup>9</sup>

The PIA,  $\tilde{g}_0(x)$ , of the magnifier may be found by substituting the appropriate form of Eq. (29) into Eq. (19b):

$$\tilde{g}_0(x) = \sum_n g_n(x) * \delta(x - Mx_n). \quad (30)$$

Substituting Eq. (16) and evaluating the resulting convolution integral [Eq. (6)] give

$$\begin{aligned} \tilde{g}_0(x) &= \sum_n g_i[x - (M - 1)x_n] \mu[x - l_n \\ &\quad - (M - 1)x_n] \mu[-x + u_n + (M - 1)x_n]. \end{aligned} \quad (31)$$

An illustration of the true and PIA outputs of the magnifier for a typical input is offered in Fig. 2 for  $M > 1$ . Each isoplanatically modeled region is "magnified" by being shifted a factor of  $M$ .

### 3. Fourier Transformer

The thin Fourier transforming lens may be viewed not only as a tool for optical information processing, but also as a space-variant linear system to which the PIA might be applied. The input-output relationship of a thin lens Fourier transformer may be expressed as

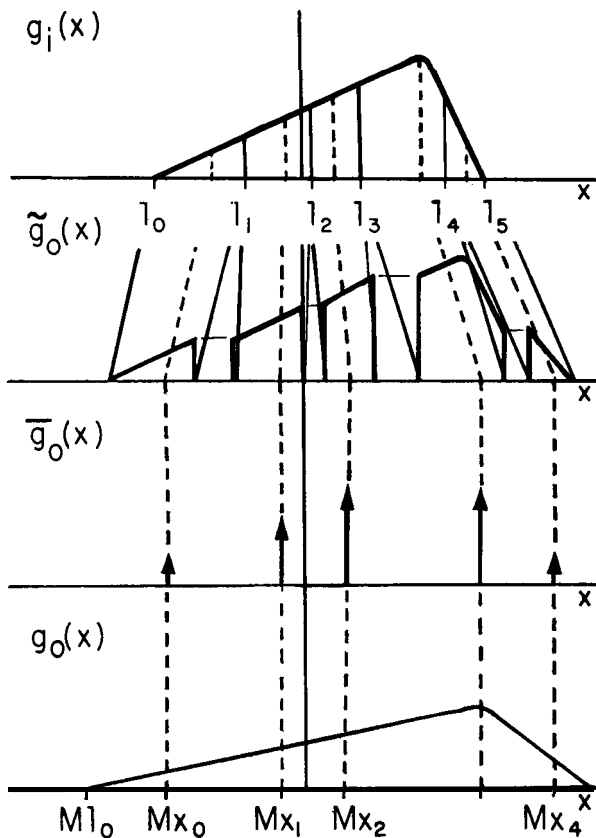


Fig. 2. Illustration of the PIA and DA outputs of the ideal magnifier [respectively,  $\tilde{g}_0(x)$  and  $\bar{g}_0(x)$ ] in contrast to the true output  $g_0(x)$  and the input  $g_i(x)$ .

$$g_0(x) = \mathcal{F}[g_i(x)] = \int_{-\infty}^{\infty} g_i(\psi) \exp\left(-j\frac{2\pi}{\lambda f} x \psi\right) d\psi, \quad (32)$$

where  $f$  is the lens's focal length and  $\lambda$  the wavelength of the spatially coherent illumination. It follows that

$$h(x - \xi; \xi) = \exp\left(-j\frac{2\pi}{\lambda f} x \xi\right). \quad (33)$$

As with the magnifier, the Fourier transformer is seen to be space variant.

The line-spread function originating from the  $n$ th isoplanatically modeled Fourier transformer input patch is

$$k_n(x) = \exp\left[-j\frac{2\pi}{\lambda f} (x + x_n)x_n\right]. \quad (34)$$

Thus

$$H_n(f_x) = \delta\left(f_x + \frac{x_n}{\lambda f}\right) \exp\left(-j\frac{2\pi}{\lambda f} x_n^2\right). \quad (35)$$

Substituting into Eq. (20) and simplifying give the Fourier domain expression of the approximated output,  $G(f_x)$ , as

$$\tilde{G}_0(f_x) = \sum_n \mathcal{F}[g_i(x + x_n)\mu(x + x_n - l_n)\mu(-x - x_n + u_n)]|_{f_x = \frac{x_n}{\lambda f}} \times \delta\left(f_x + \frac{x_n}{\lambda f}\right). \quad (36)$$

Inverse transforming yields

$$\tilde{g}_0(x) = \sum_n \mathcal{F}[g_i(x + x_n)\mu(x + x_n - l_n)\mu(-x - x_n + u_n)]|_{f_x = \frac{x_n}{\lambda f}} \times \exp\left(-j\frac{2\pi}{\lambda f} x_n x\right). \quad (37)$$

This is the general statement of the PIA for a Fourier transformer.

Equation (36) bears a remarkable computational resemblance to a Fourier series spectrum. The Fourier series spectrum  $G(f_x)$  for a periodic function  $g(x)$  with period  $(u - l)$  may be written

$$G(f_x) = \sum_n \mathcal{F}[g_i(x)\mu(x - x_0 - l)\mu(-x + x_0 + u)]|_{f_x = nf} \times \delta(f_x - nf), \quad (38)$$

where  $x_0$  is any point on the  $x$  axis, and  $f = 1/(u - l)$ . Both the Fourier transform PIA and the Fourier series spectrum are expressed in the frequency domain as impulse trains weighted by a Fourier transform expression of the function to be synthesized.

For a specific example of application of the Fourier transformer PIA, consider the transformer input of a spatial pulse:

$$g_i(x) = \mu(x + a)\mu(a - x), \quad (39)$$

where  $2a$  is the pulse width. The true output would be

$$g_0(x) = 2a \operatorname{sinc}(2ax/\lambda f), \quad (40)$$

where

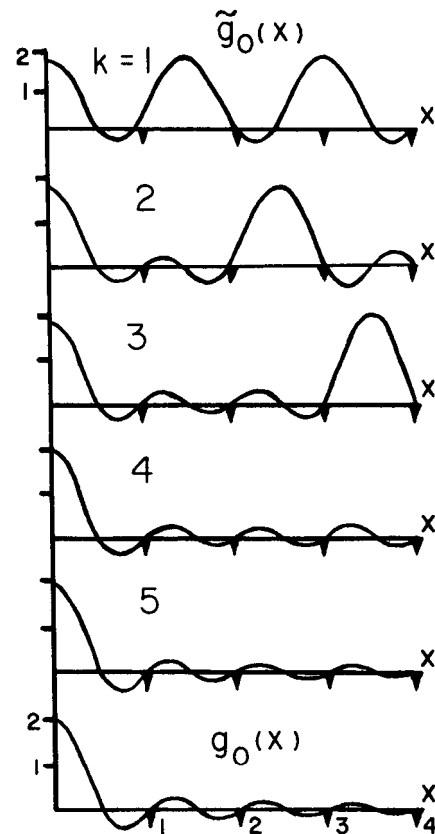


Fig. 3. The PIA's of the Fourier transformer output to a rectangular pulse input divided into  $2k + 1$  isoplanatic patches compared to the true output  $g_0(x)$ .

$$\text{sinc}(x) = [\sin(\pi x)]/(\pi x). \quad (41)$$

To apply the PIA, we arbitrarily divide the input pulse into  $2k + 1$  isoplanatic patches all of width  $w$  such that

$$w = u_n - l_n = 2a/(2k + 1). \quad (42)$$

Let  $x_n$  be the midpoint of the  $n$ th patch so that

$$x_n = (u_n + l_n)/2. \quad (43)$$

The  $n$ th isoplanatic region of the input pulse is then

$$g_n(x) = \mu\left(x + \frac{w}{2}\right)\mu\left(\frac{w}{2} - x\right). \quad (44)$$

Substitution into Eq. (37) followed by simplification gives

$$\tilde{g}_0(x) = w \left[ 1 + 2 \sum_{n=1}^k \text{sinc}\left(\frac{nw^2}{\lambda f}\right) \cos\left(\frac{2n\pi wx}{\lambda f}\right) \right] \quad (45)$$

An illustration of the convergence of this approximate output to the true output [Eq. (40)] is offered in Fig. 3 with  $\lambda f = a = 1$  for  $k = 1, 2, 3, 4$ , and 5.

#### IV. Discrete Approximation

Deen, *et al* have employed an input plane sampling technique to approximate space-variant system outputs. The input is sampled according to

$$g_s(x) = \sum_n g_i(x_n)\delta(x - x_n), \quad (46)$$

where  $g_i(x)$  denotes the sampled input. The corresponding output, from Eqs. (3) and (14), is the discrete form of the superposition integral [Eq. (3)]:

$$\bar{g}_0(x) = \sum g_i(x_n)h_n(x - x_n). \quad (47)$$

Here,  $\bar{g}_0(x)$  denotes the discrete approximation (DA) of the variant system output.

For purposes of comparing to the true and PIA outputs, the DA output for an ideal imaging system with magnification  $M$  [from Eqs. (14), (29), and (47)] is

$$\bar{g}_0(x) = \sum_n g_i(x_n)\delta(x - Mx_n). \quad (48)$$

An example for a typical input is offered in Fig. 2.

The DA is recognized as a special case of the PIA when inputs (1) are restricted to weighted impulse trains [Eq. (46)], (2) consist of a single impulse per

isoplanatic patch, and (3) have line-spread functions determined from each input impulse location.

#### V. Conclusions

The superposition integral approximations presented herein may be used to approximate the outputs of linear space-variant systems. Employment of the discrete approximation (DA) for representing the space-variant nonunity magnification imaging system has been reported in the literature.

The piecewise isoplanatic approximation of which the DA is a special case, arises from division of the space-variant system input plane into a number of isoplanatic patches. Each input patch is treated as an individual space-invariant linear system. The outputs resulting from each patch are summed to give the PIA output of the simulated system.

The effectiveness of the PIA is illustrated by its application to the ideal magnifier and Fourier transformer. The invariant system modeled as piecewise isoplanatic is shown to produce equivalent true and PIA outputs as exemplified by the differentiator.

Space-variant system output approximations lay the system theory foundation for holographic representation (and thus real space condensation) of multielement linear space-variant systems.

#### References

1. L. C. Burton, M. O. Hagler, and T. F. Krile, *IEEE J. Quantum Electron.* QE-9, 633 (1973); paper presented at the IEEE/OSA Conference on Laser Engineering and Applications, Washington, D.C. (30 May-1 June 1973).
2. L. M. Deen, M. O. Hagler, and J. F. Walkup, *J. Opt. Soc. Am.* 64, 1396A (1974); paper presented at the 1974 Annual Meeting, Optical Society of America, Houston, Texas, 15-18 October 1974.
3. L. M. Deen, "Holographic Representations of Optical Systems," M.S. thesis, Department of Electrical Engineering, Texas Tech University, Lubbock, Texas (January 1975).
4. L. M. Deen, J. F. Walkup, and M. O. Hagler, *Appl. Opt.* 14, 2438 (1975).
5. R. J. Marks II, "Holographic Recording of Optical Space-Variant Systems," M.S. thesis, Rose-Hulman Institute of Technology, Terre Haute, Indiana (August 1973).
6. P. B. Fellgett and E. H. Linfoot, *Philos. Trans. R. Soc. London* A247,369 (1955).
7. J. W. Goodman, *Introduction to Fourier Optics* (McGraw-Hill, New York, 1968).
8. A. W. Lohmann and D. P. Paris, *J. Opt. Soc. Am.* 55, 1007 (1965).
9. A. A. Sawchuk, *J. Opt. Soc. Am.* 64,138 (1974).

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